

Product Readiness Review

Diamond Turning Machine Assembly

Team 1 a.k.a Team K.I.S.S

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11/11/2010

MAE 491-01 Product Realization

Instructor - Dr. Christina Carmen

Customer - Tim Blackwell

Advisor - Steve Collins

Sponsor - Hubbard and Drake General Mechanical Contractors

Overview

- Purpose of PRR
- Mission Statement
- Product Design Specifications
 - Design Drawings
 - Technical Analysis
 - Verification Tests
 - Final Cost Analysis
- Manufacturing/Assembly/Installation
 - Problems and Solutions
 - Lessons Learned
 - Summary

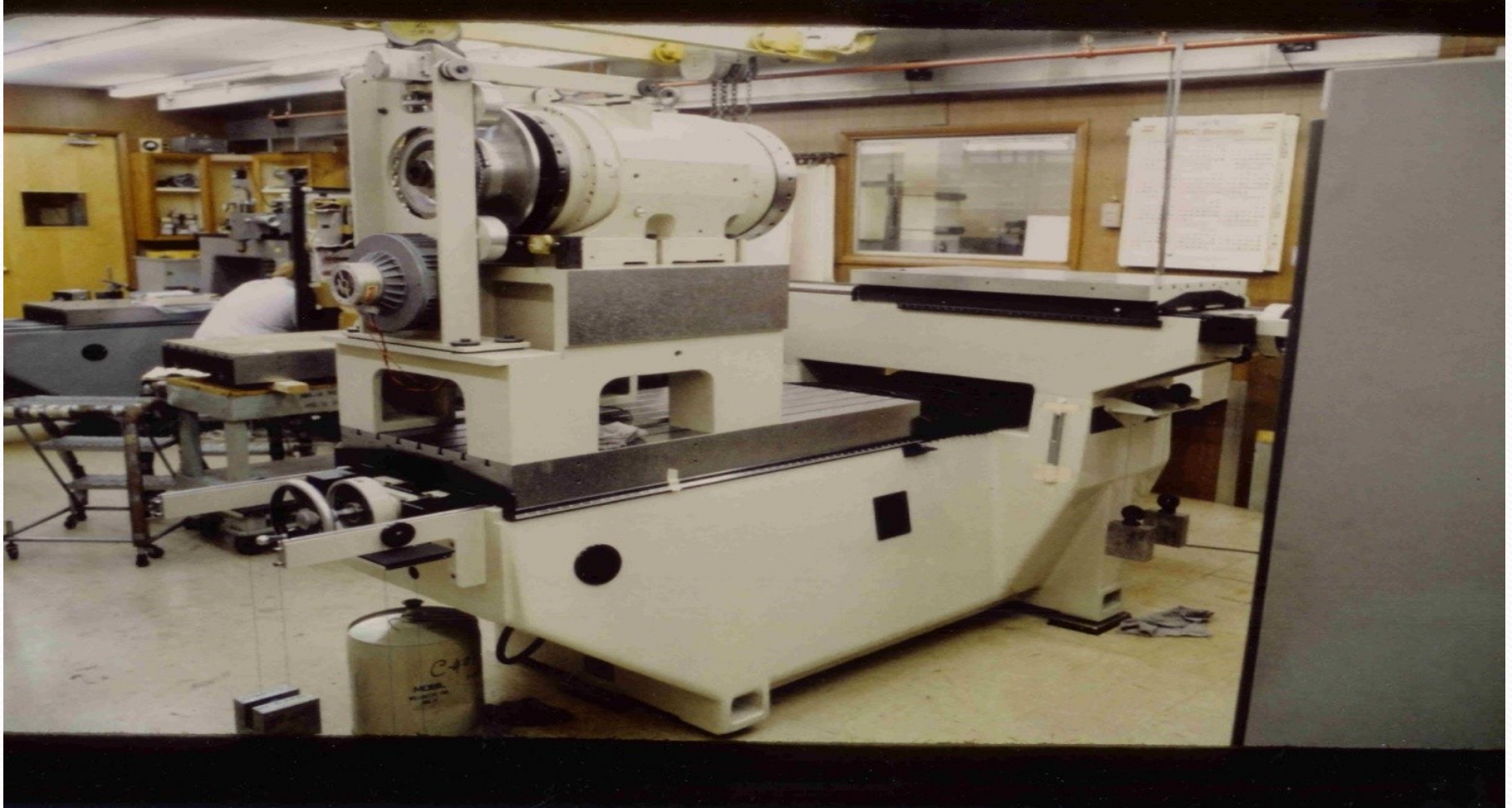
Purpose of PRR

- Review the results of the system verification processes
- Provide Final Cost information
- Demonstrate product to verify it meets the product design specifications

Mission Statement:

To design a lifting system for the Center for Applied Optics at UAHuntsville that will be able to properly and safely lift and lower two slides of a Moore 30" diameter Diamond Turning Machine, from their packaged state onto the machine. The system must be able to rotate the slides 180 degrees and set the slides down softly to avoid denting the precision burnished slide grooves.

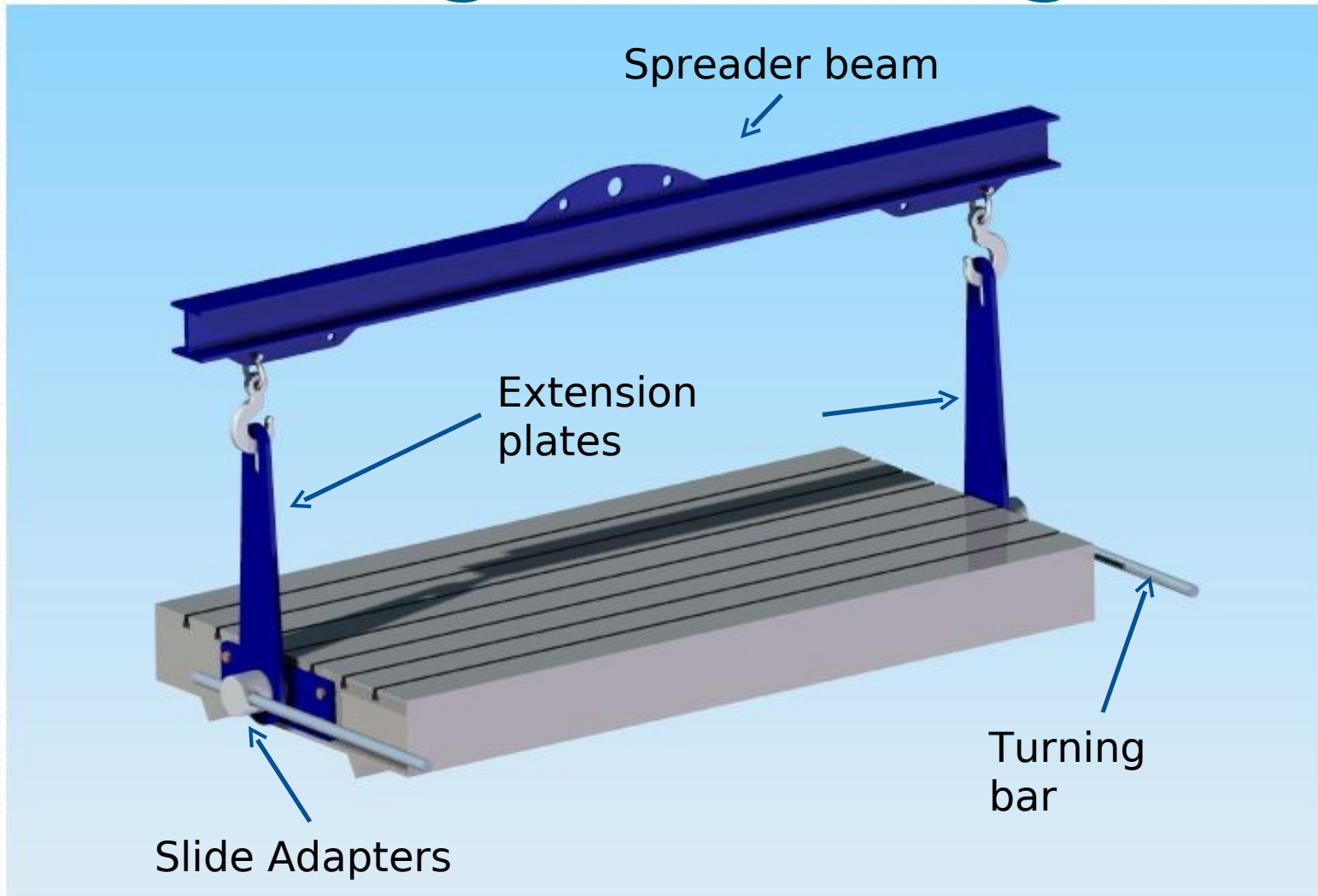
Diamond Turning Machine



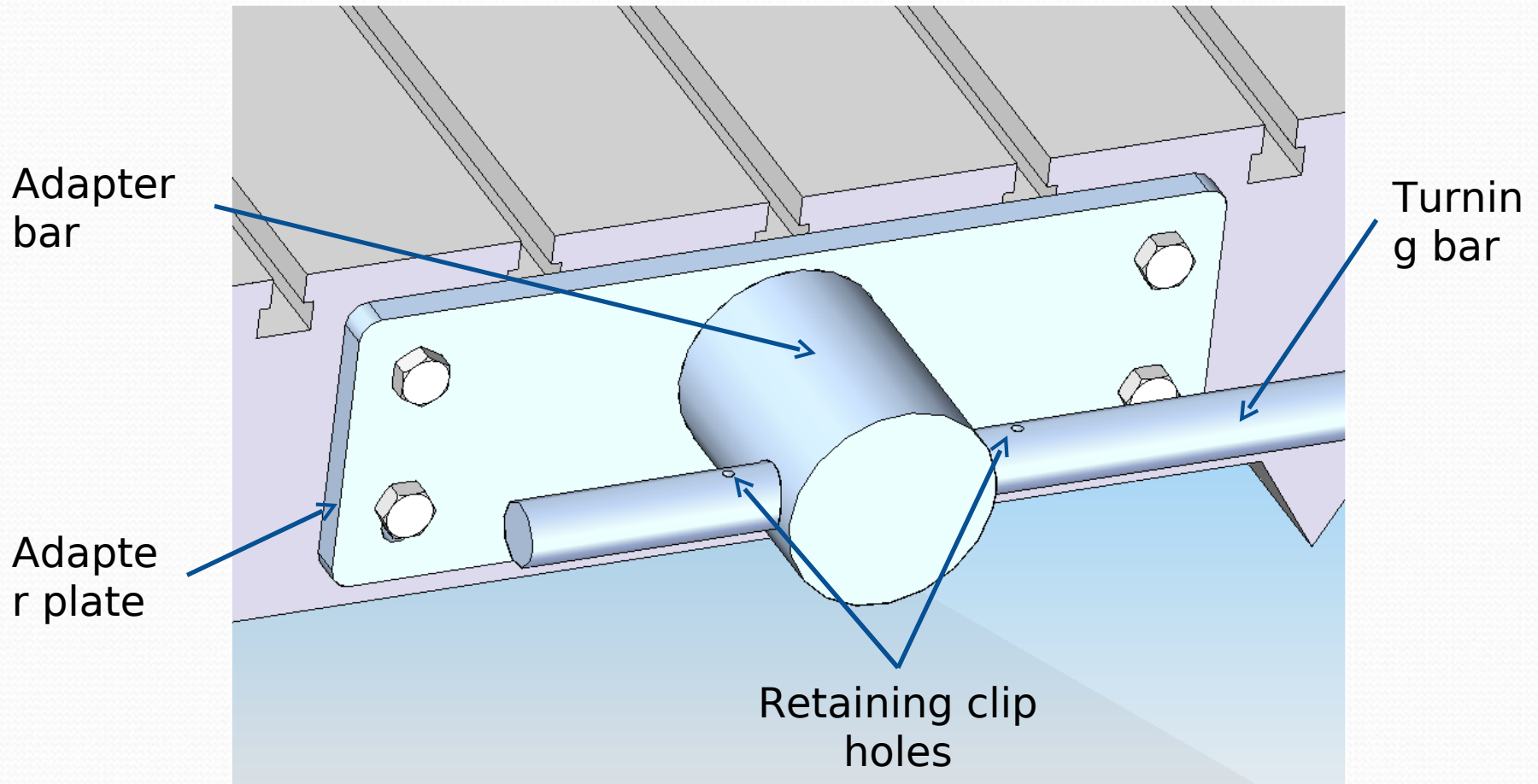
Product Design Specifications

- The lifting beam must be able to attach to a fork lift or a cherry picker like device.
- The device to which the beam is attached must be able to lower the beam slow enough not to damage the machine as well as mobile enough to be moved into the proper position.
- The beam must be able to support the weight of the slides as well as rotate them 360 degrees
- There should be a factor of safety of at least 2 for all designed loads.

Design Drawings

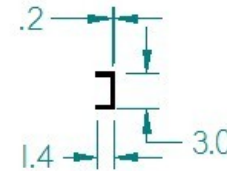
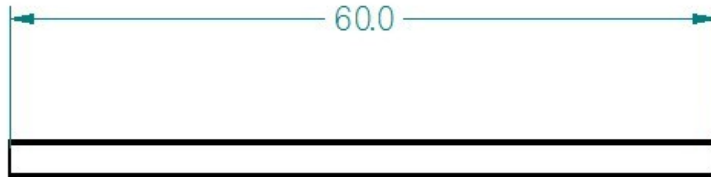
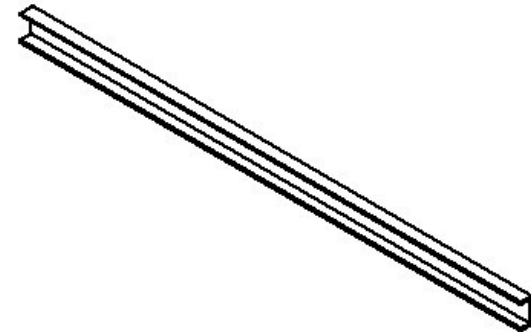


Design Drawings



Design Drawings – C channel

Material 3 in. steel C channel (2 pcs)
 All dimensions in inches.



REVISION HISTORY			
REV	DESCRIPTION	DATE	APPROVED

DATE	NAME	SCALE	HEIGHT	SET OFF

SOLID EDGE
 Job: The S. Company

DESIGN		DATE	
ISSUED			

UNLESS OTHERWISE SPECIFIED
 DIMENSIONS ARE IN INCHES
 ANGLES NOT

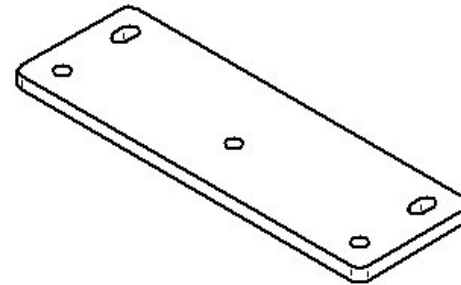
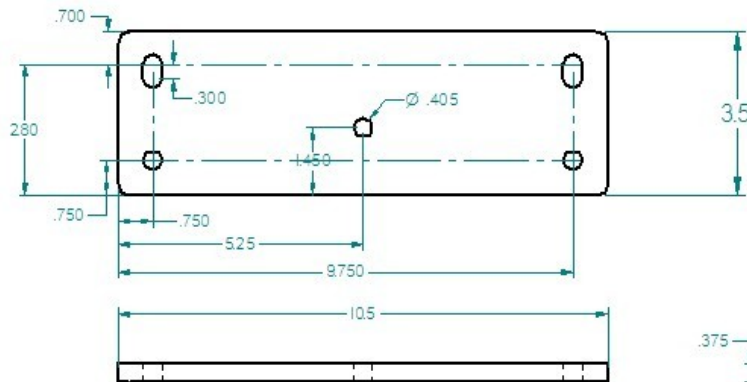
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Design Drawings – Adapter plate

Material: Mild Steel plate

All dimensions in inches

All Holes and slots 0.405 in dia.
for 3/8 bolt clr.



REVISION HISTORY			
REV	DESCRIPTION	DATE	APPROVED

DATE	NAME	DATE	NAME
07/15/10	Shannon	07/15/10	PLK

SOLID EDGE
©2007 The PTC Company

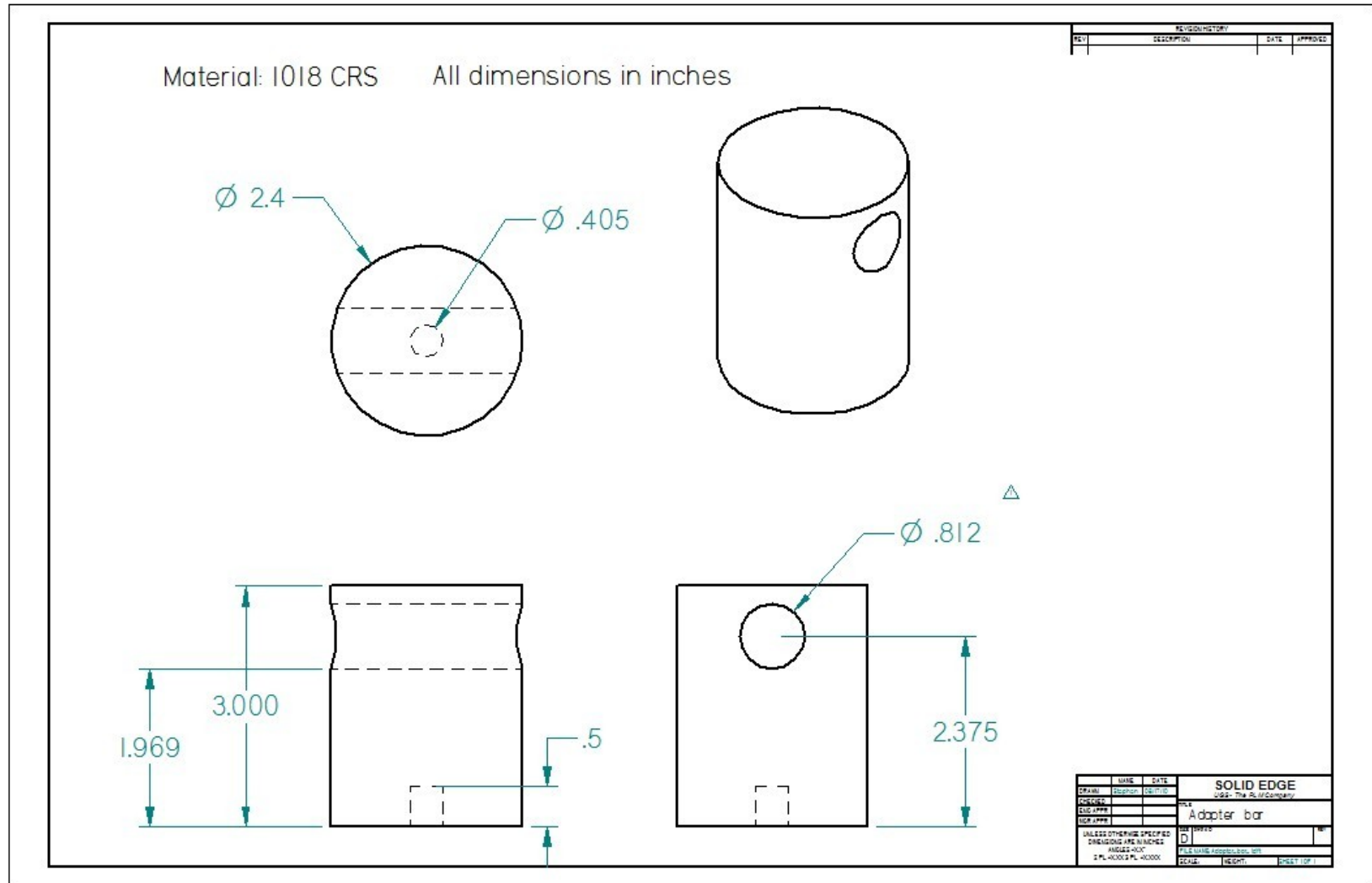
Adapter plate

UNLESS OTHERWISE SPECIFIED
DIMENSIONS ARE IN INCHES
ANGLES IN DEGREES

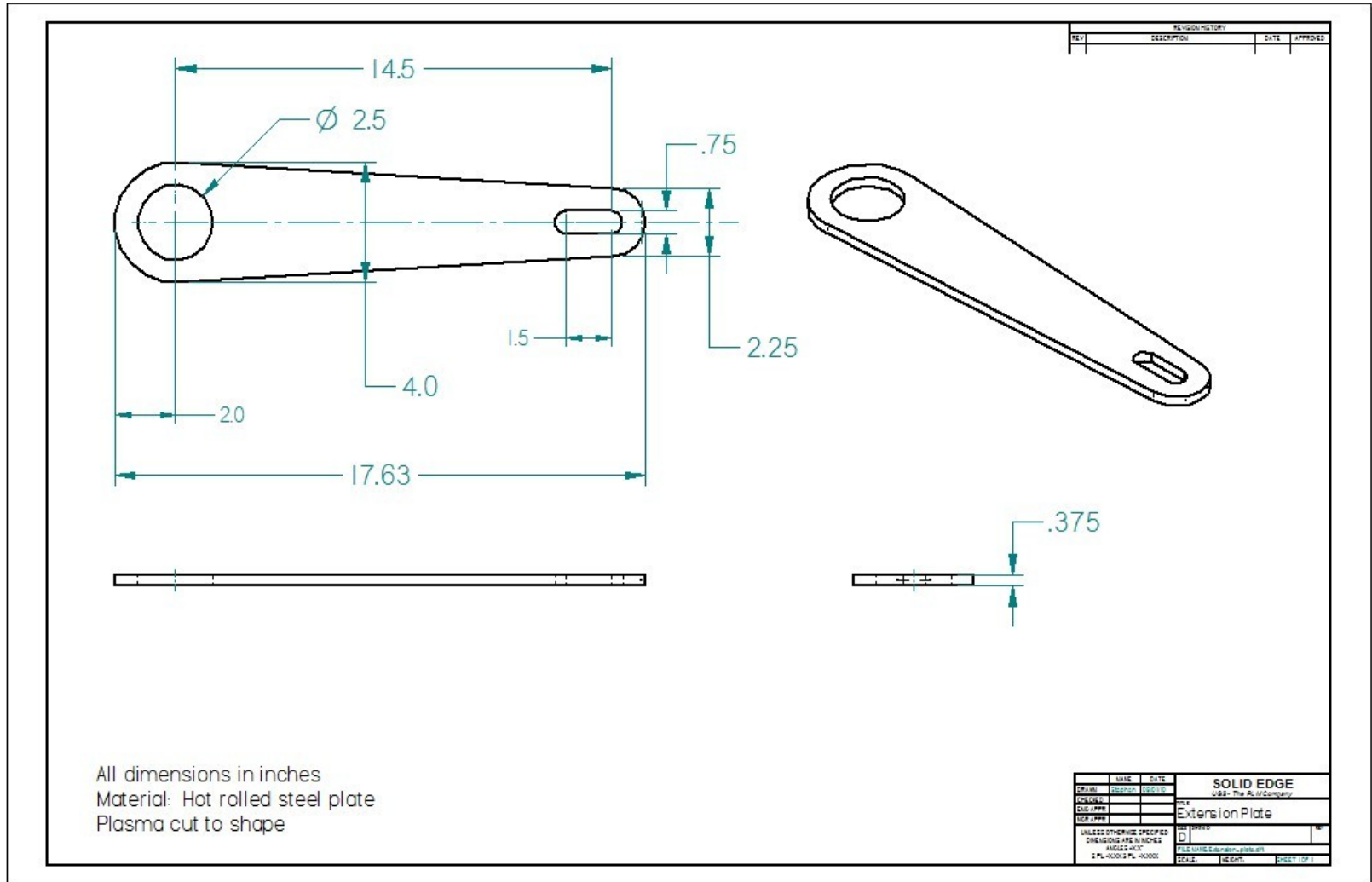
1 PL-00002-PL-00000

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SHEET 1 OF 1

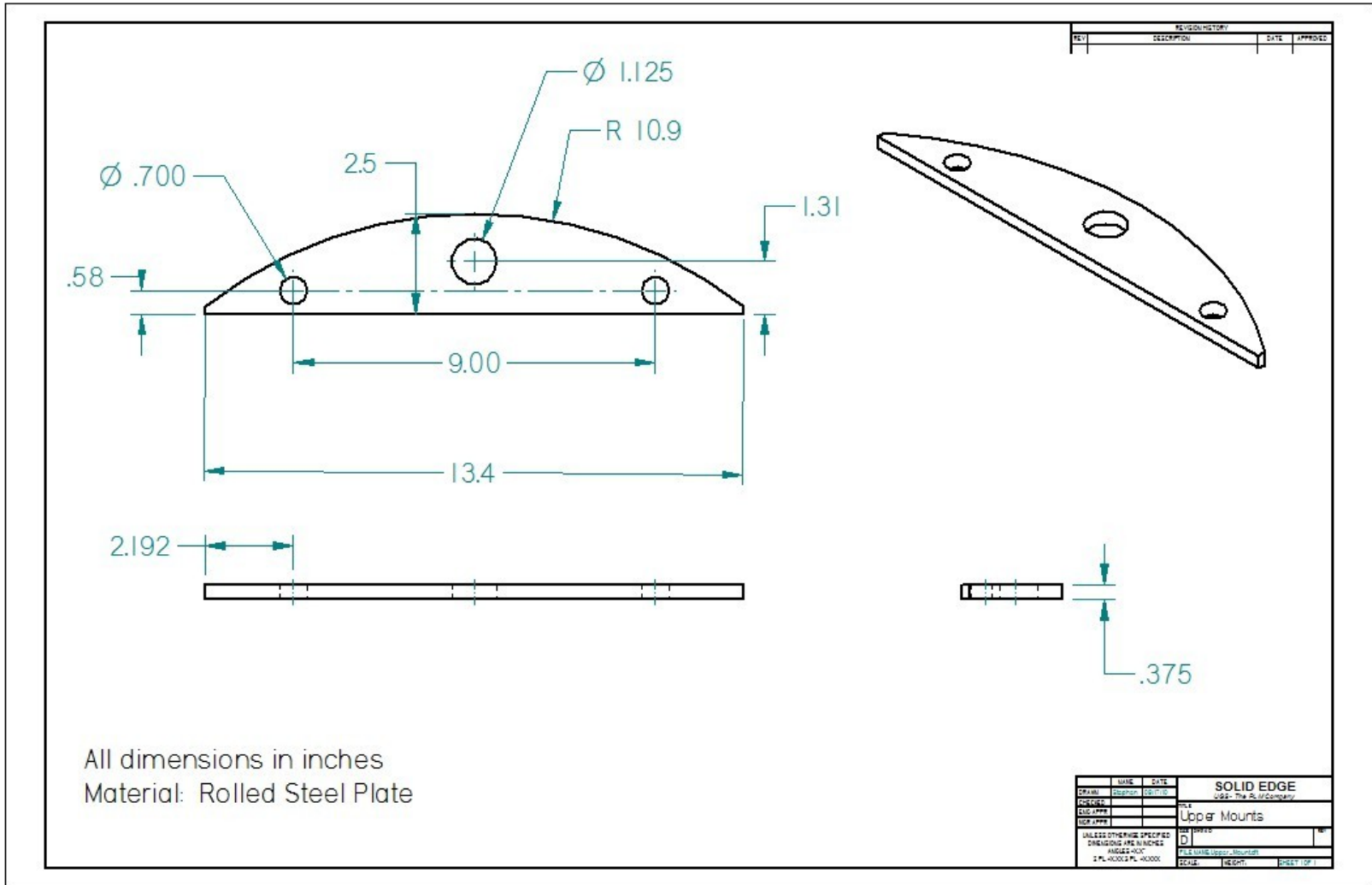
Design Drawings – Adapter bar



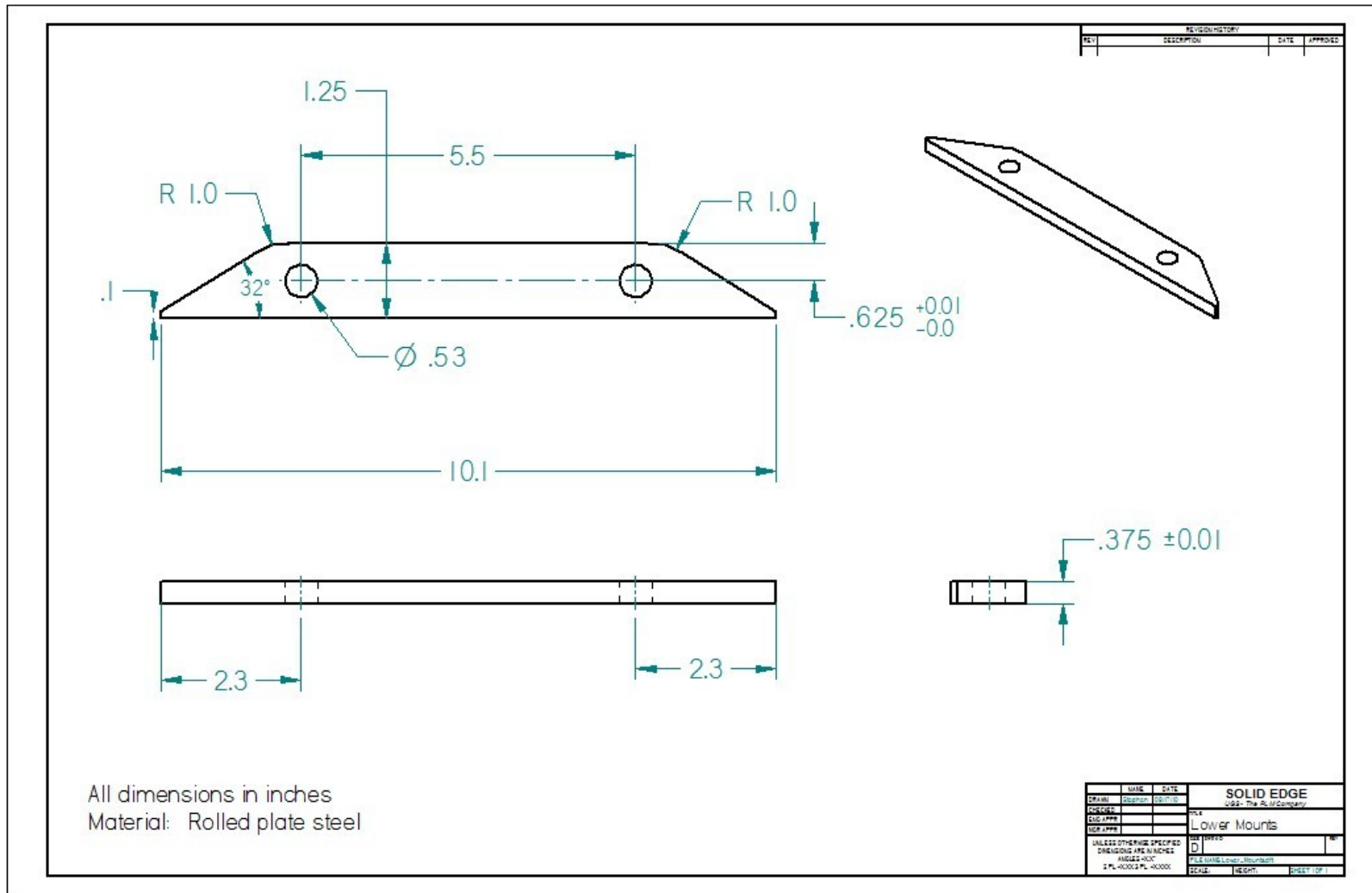
Design Drawings - Ext. Plate



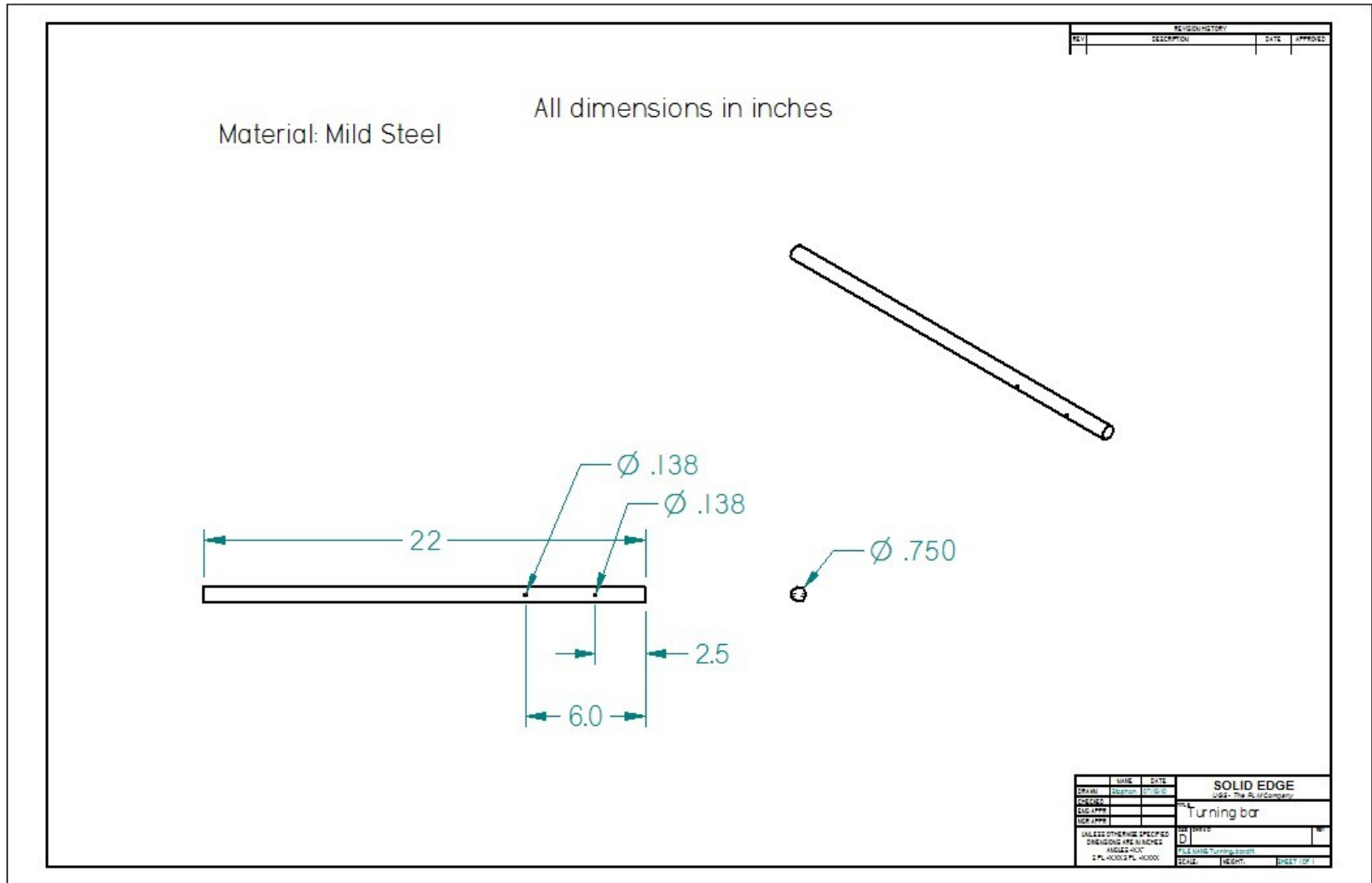
Design Drawings - Upper Mts.



Design Drawings - Lower Mts.



Design Drawings – Turning bar



Technical Analysis

Nastran FEA Results

These are the results for the simple 1-D analysis of just an I beam under two different load cases.

Fork-truck loading

- Maximum stress of 3760 psi compared to hand calculation of 3755 psi
- Percent diff. of 0.1%
- Maximum deformation of 0.025 in

Engine hoist loading

- Maximum stress of 4780 psi compared to hand calculation of 4769 psi
- Percent diff. of 0.2%
- Maximum deformation of 0.026 in

Technical Analysis

C-Channel Beam Rev. A

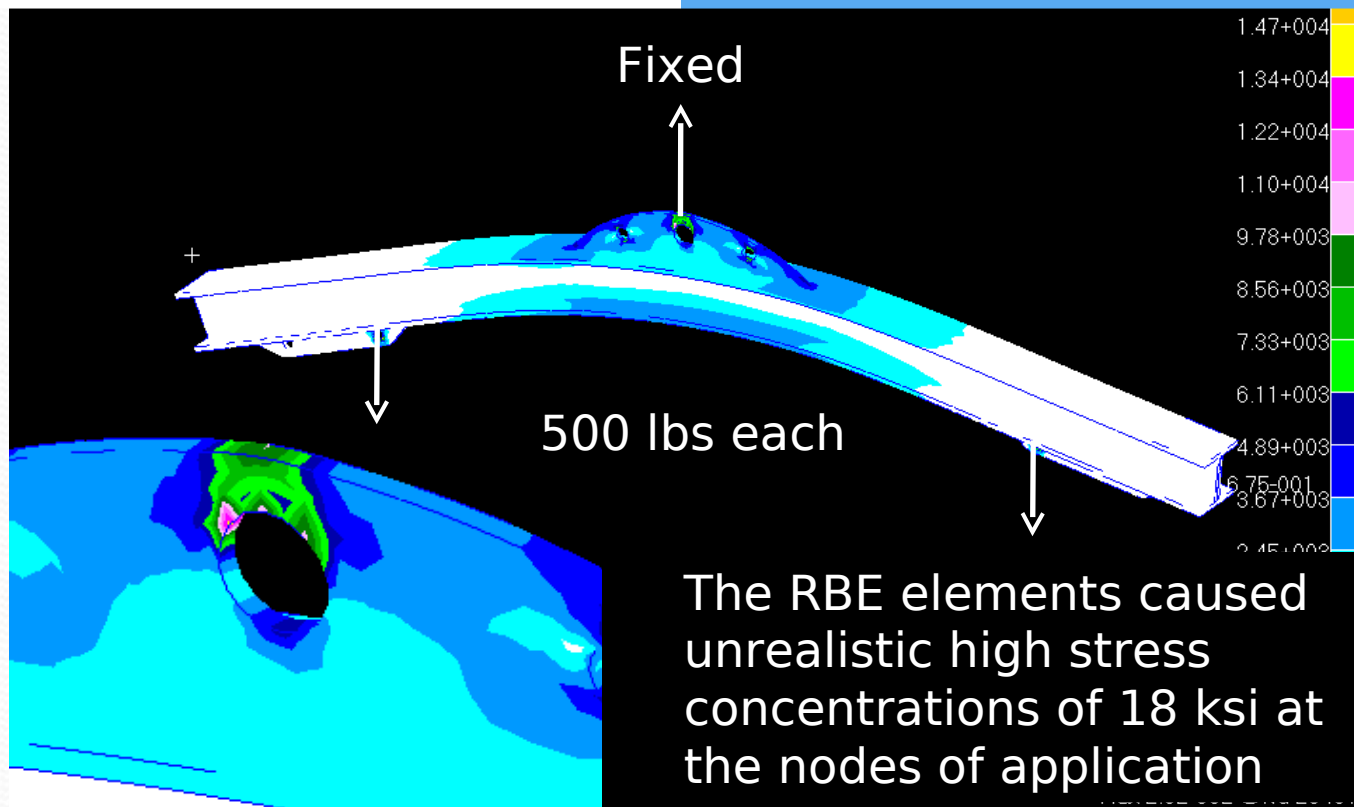
- A special Solid Edge Model was created to mimic the welded geometry in order to analyze the new spreader beam weldment.
- Rigid body elements were then used to constrain the large hole where the hook is placed and to apply forces to the holes in the lower mounts.

Technical Analysis

Engine Hoist Loading

The green stresses of approx. 10 ksi near the hook hole are most likely near realistic values.

The med. Blue areas compare closely to the values obtained with the 1-D analysis

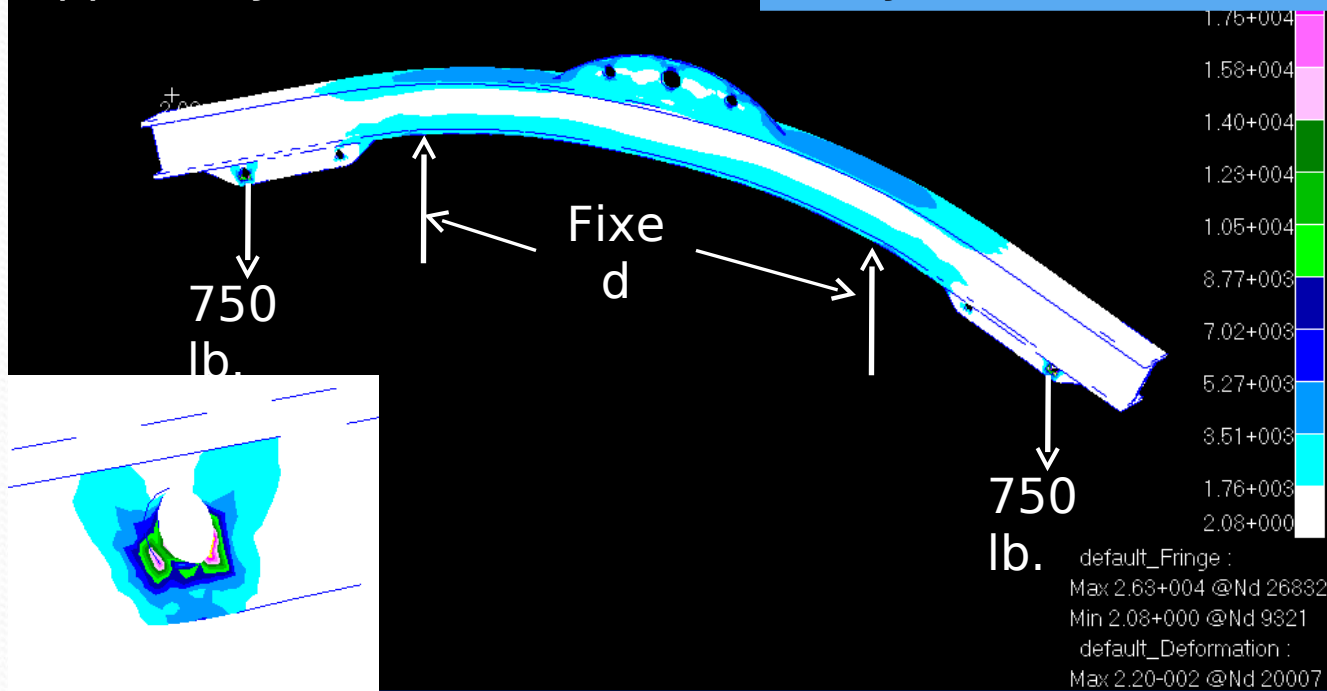


Technical Analysis

Fork truck Loading

This model also had unrealistic high stress concentrations of 26 ksi where the 750 lb forces were applied by RBE elements.

The med. Blue areas also compare closely to the values obtained with the 1-D analysis



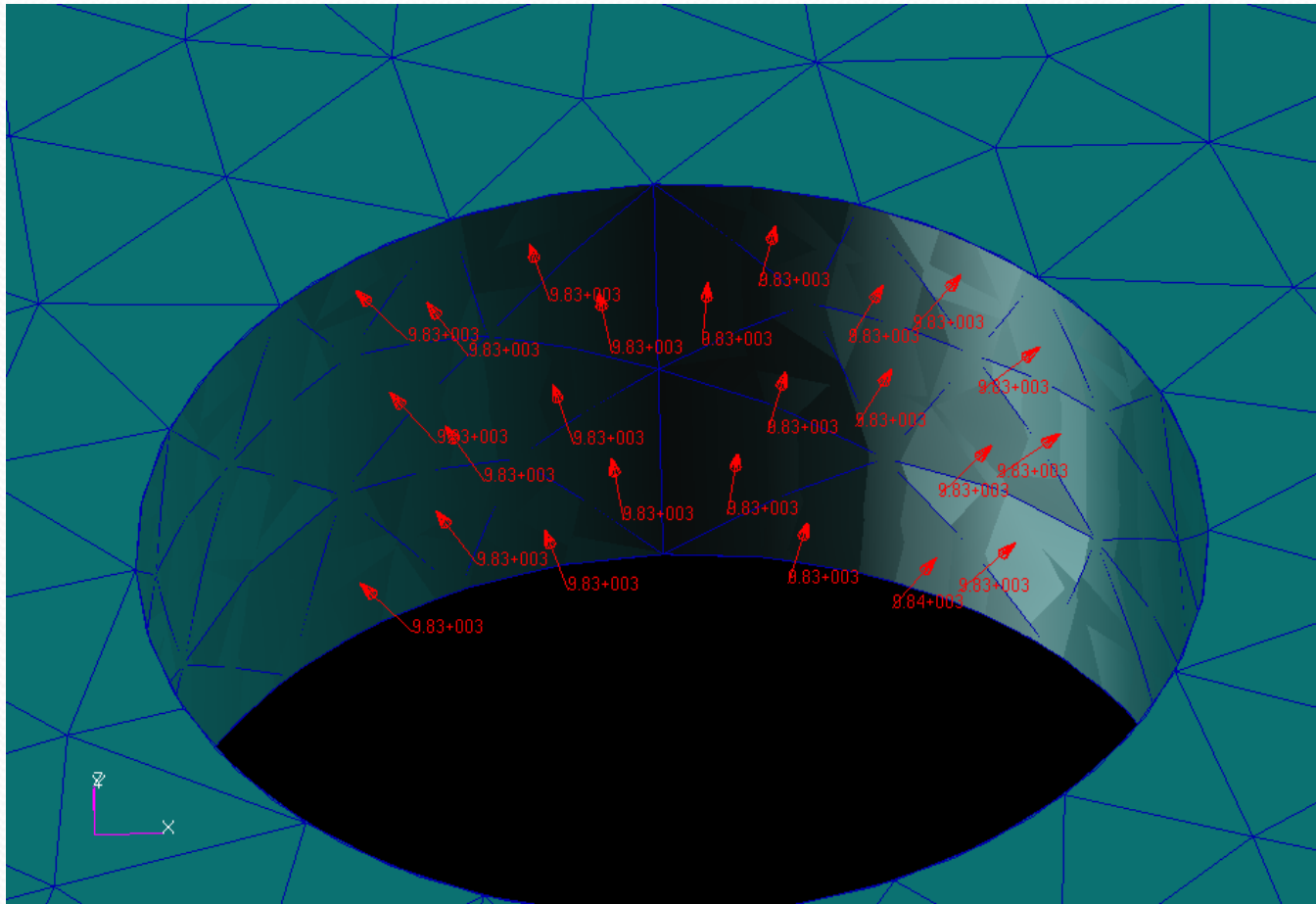
Technical Analysis

Mounting plates

- In order to better represent the loads imposed at the hole locations of the upper and lower mounting plates, separate FEAs were done using load application by pressure instead of point force methods.
- After meshing the model, the actual size of individual elements was used to create a pressure function that could be applied to the contact surfaces inside the holes.
- Both models were constrained by fixing the areas that were to be welded to the beam.

Technical Analysis

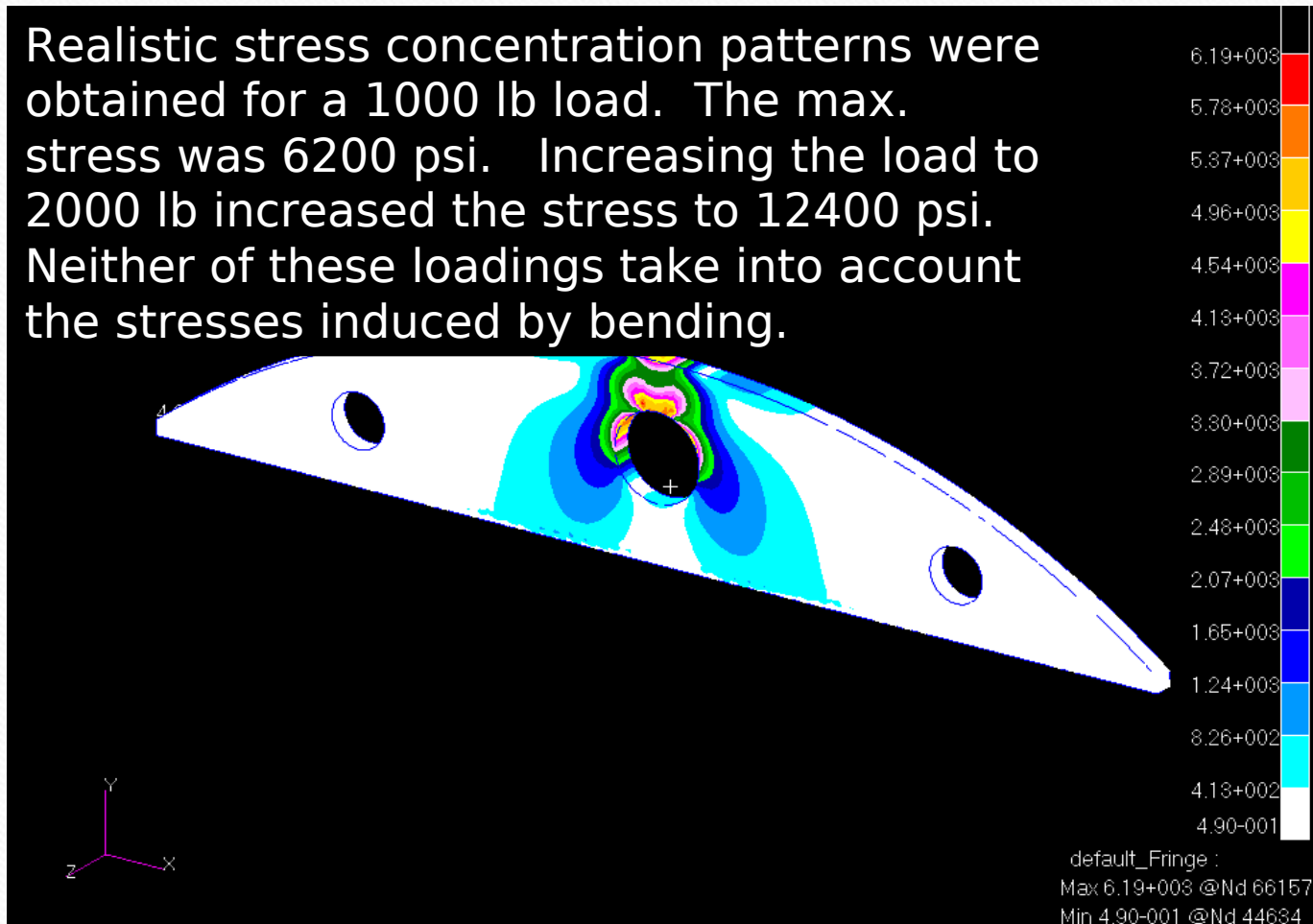
Typical Pressure Load Application



Technical Analysis

Upper Mount (Engine Hoist Loading)

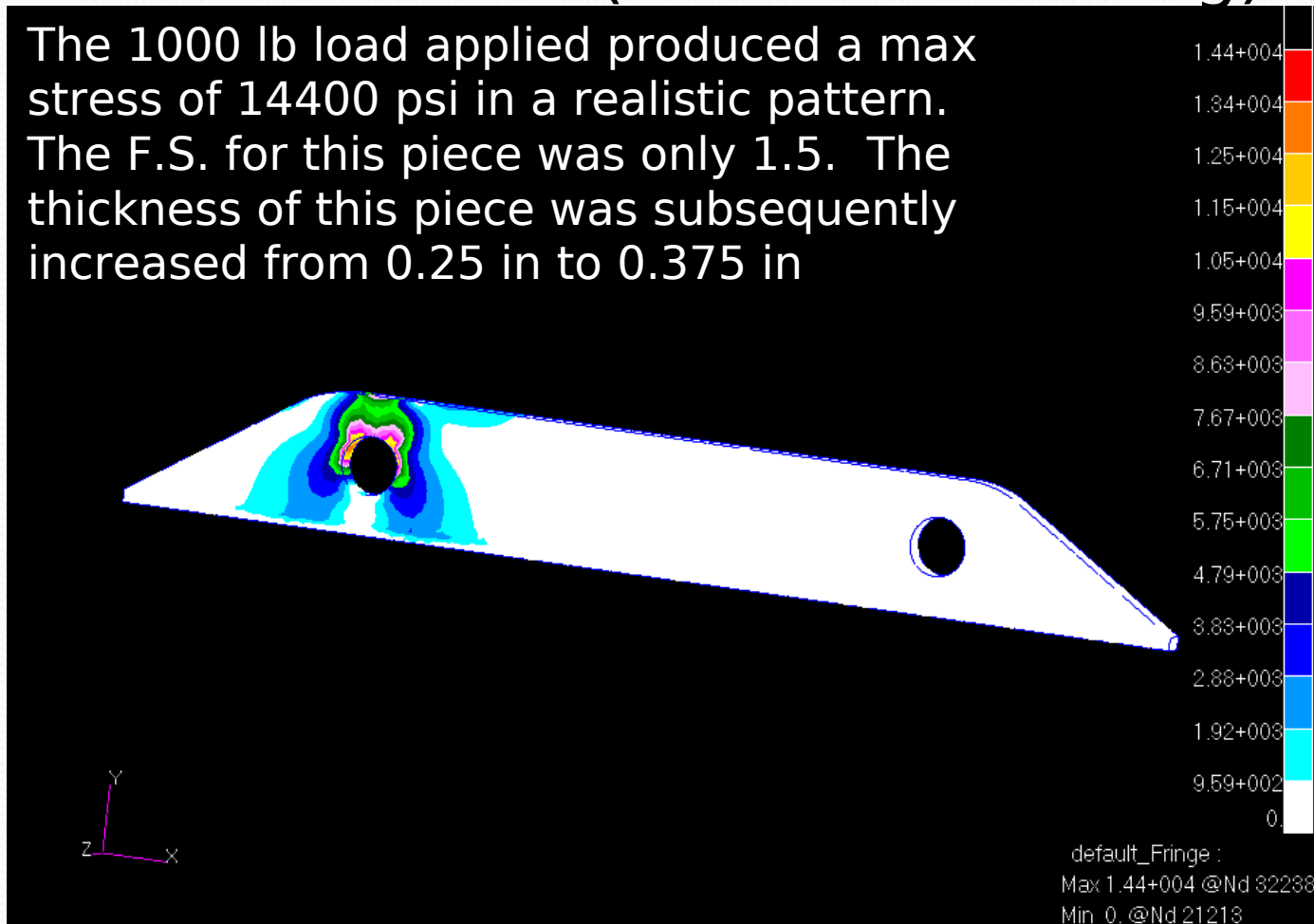
Realistic stress concentration patterns were obtained for a 1000 lb load. The max. stress was 6200 psi. Increasing the load to 2000 lb increased the stress to 12400 psi. Neither of these loadings take into account the stresses induced by bending.



Technical Analysis

Lower Mounts (Fork Lift Loading)

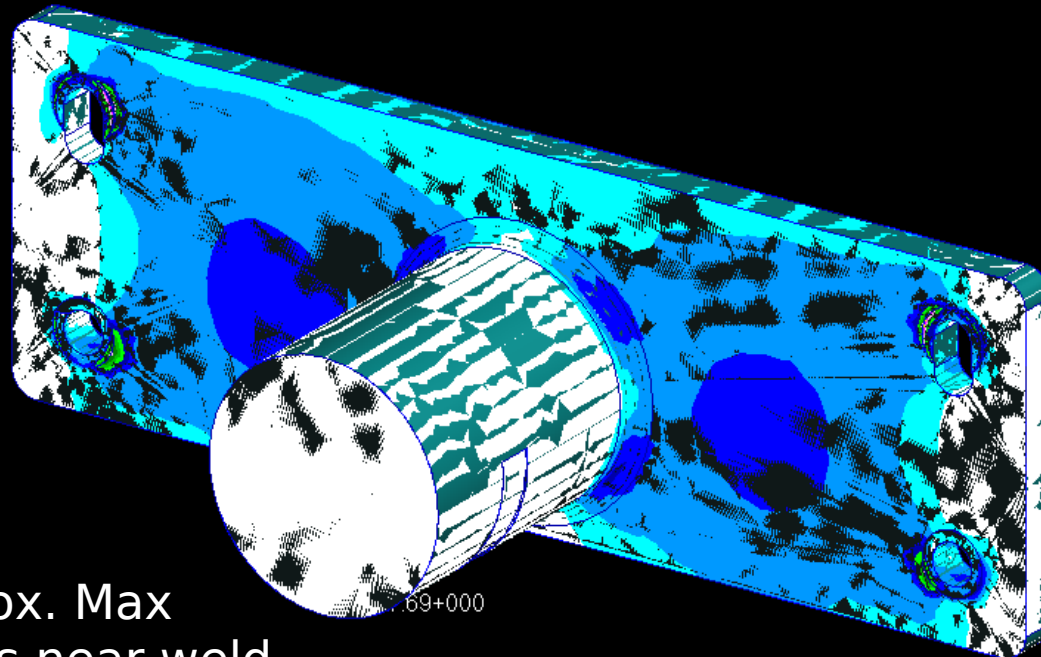
The 1000 lb load applied produced a max stress of 14400 psi in a realistic pattern. The F.S. for this piece was only 1.5. The thickness of this piece was subsequently increased from 0.25 in to 0.375 in



Technical Analysis

Adapters

Max. Stresses of 18 ksi near bolt holes is not realistic because of fixed surface constraints

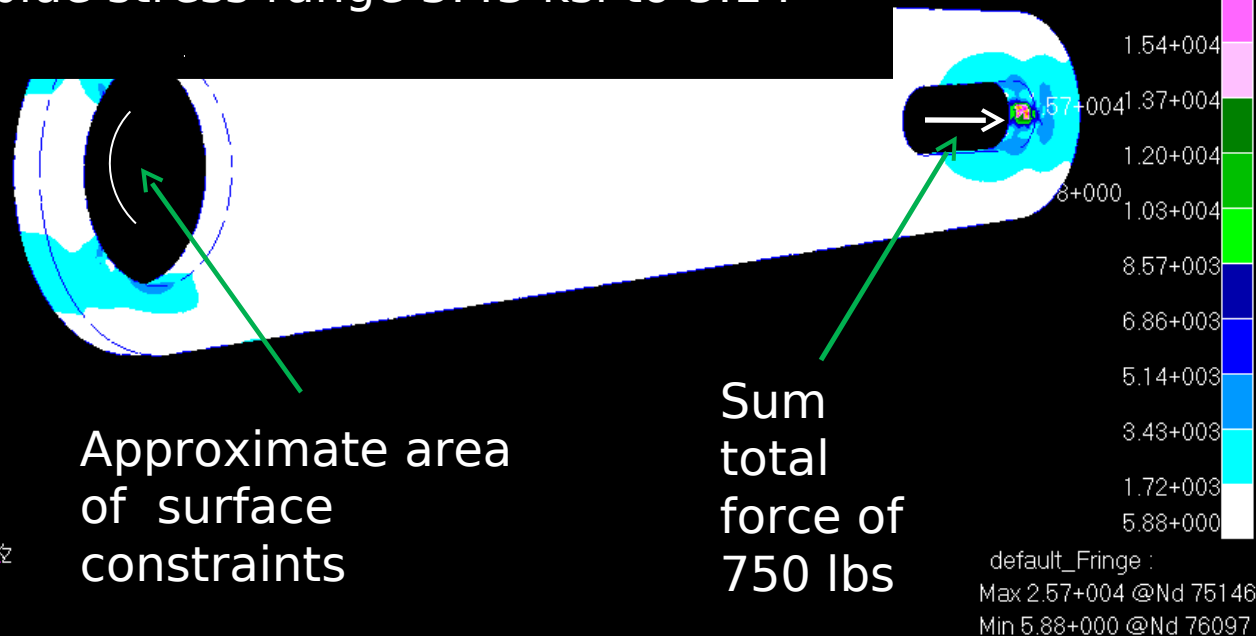


Approx. Max
Stress near weld
areas is 6000 psi

Technical Analysis

Extension Plates

The 8 point force loads mimic the plate resting on 8 spikes. Stresses in this area are unrealistic
Light blue stress range 1.72 ksi to 3.43 ksi
Med blue stress range 3.43 ksi to 5.14 ksi



Verification Tests

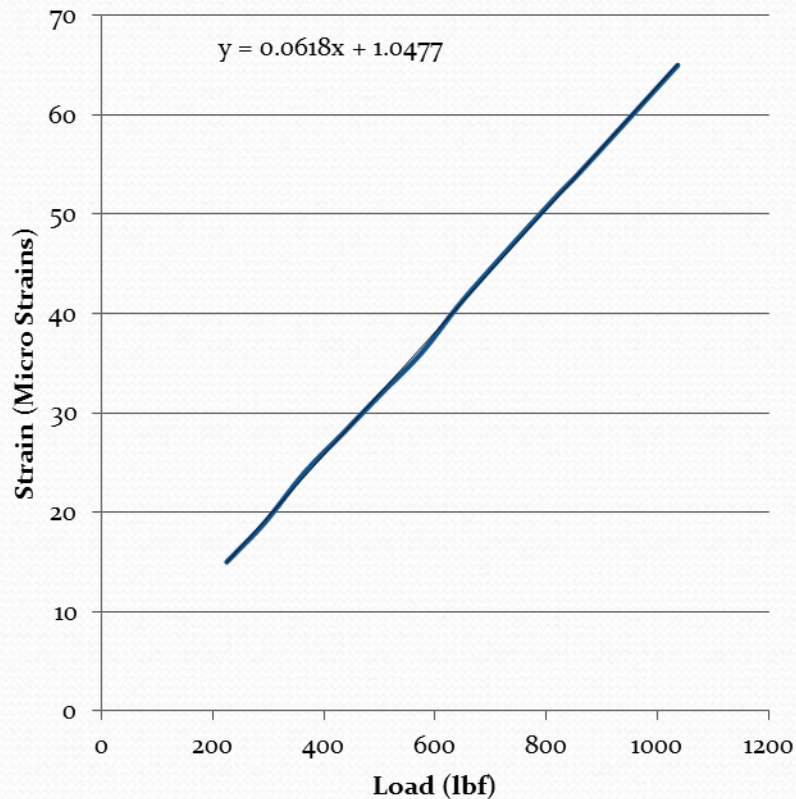
- Verification was performed using strain gauges and loading the beam in a controlled environment.
- The beam was progressively loaded to 1000lbs, recording strain in critical locations determined from FEA analysis.
- A plot of load vs. strain was used to later find the weight of the slide.
- The curve obtained was also used to determine stress in the beam with our 2000 lb maximum load.

Verification Tests

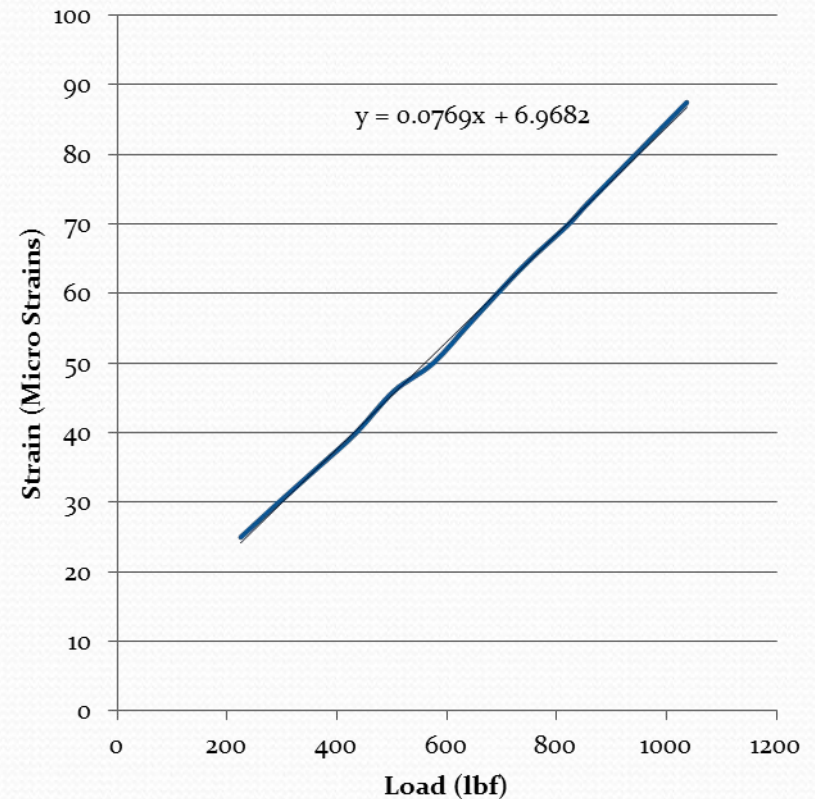
- Hooke's Laws were used to find stress from the strain recorded.
- The reduced equation of $\sigma = E\varepsilon$ gave a maximum stress of 5000 psi along the top surface of the beam. This gives a factor of safety of $FS = \frac{Load_{Max}}{Load} = \frac{36000}{5000} = 7.2$
- The weight found from the data for the large slide was 1130 lbs. This value is much lower than was found using CAD modeling and is most likely incorrect since the load was applied at an angle in respect to the mounts on the beam during the tests.

Verification Tests

Hoop (Fork Truck)

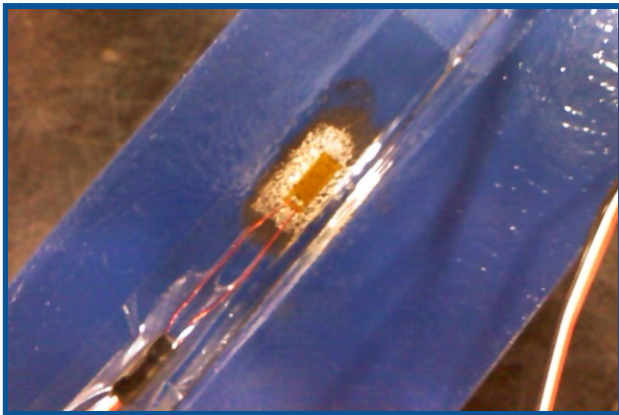
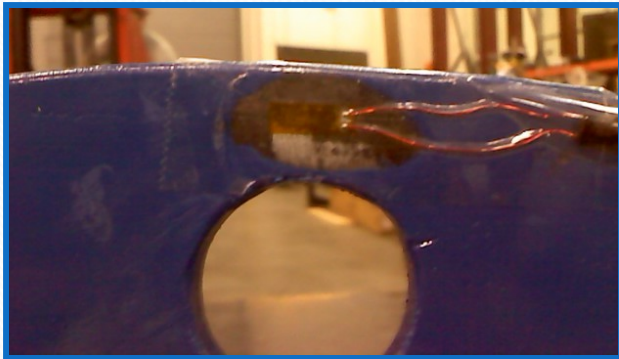


Beam Top (Fork Truck)



Verification Tests

Strain Gauges



Loading the beam with 1000 pounds of stuff



Preparing Slides



Bolting Bearings to Slide

Preparing Machine



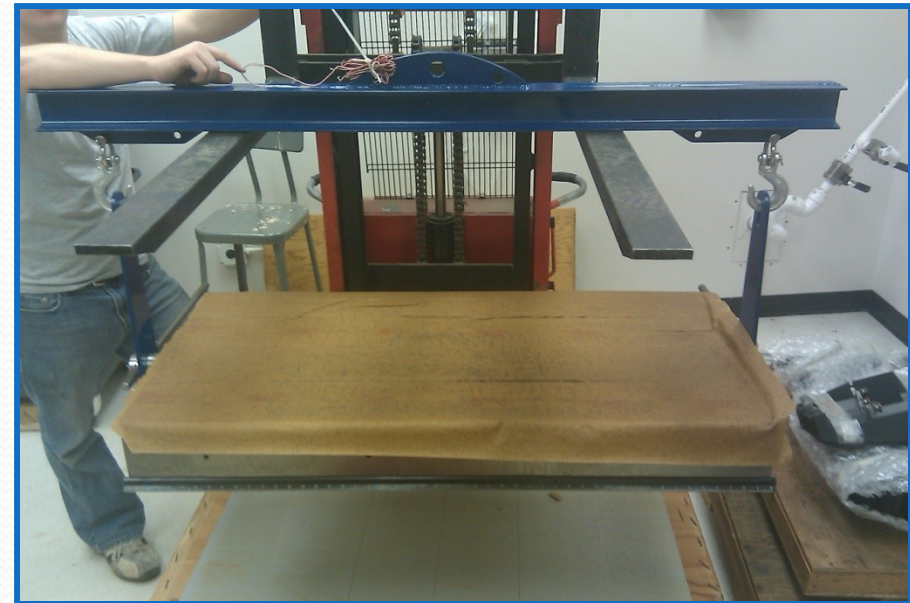
Cleaning Bearings

Pouring oil For slide channel



Lifting Slides

Slide Lifted and Rotated



Video



Updated Cost Analysis

Cost Analysis

Materials Cost

Design type	Material description	Price per unit	units	Retail Cost	Actual Cost	Supplier	Actual Supplier
C channel Rev A	3 X 1-3/8 X 3/16 Steel Channel 6 ft. L	\$28.26	2	\$57	\$0	Metal Depot	Stephen Armstrong
	3/8 x 2ft x 2ft flat plate	\$77.20	1	\$77	\$0	Metal Depot	Hubbard and Drake
	3/8 slip hook (5400 lb rating)	\$10.58	2	\$21	\$21	Grainger	Grainger
	3/8 shackle (1700 lb rating)	\$5.69	2	\$11	\$11	Home Depot	Home Depot
	3/8 x 16 x 1.25 in grade 8 bolts	\$0.71	8	\$6	\$6	Home Depot	Home Depot
			Subtotal	\$172	\$38		
Slide Adapters	3/4 in steel round stock (4 ft)	\$8.24	1	\$8	\$0	Metal Depot	Hubbard and Drake
	1/8 quick clips for turning bar	\$1.06	4	\$4	\$4	Lowe's	Lowe's
	2.5 in steel round stock (1 ft)	\$27.94	1	\$28	\$0	Metal Depot	Hubbard and Drake
				Subtotal	\$40	\$4	

Hardware Cost

Fork lift Modifications

Hardware description	Price per unit	units	Retail Cost	Actual Cost		
Instrumentation quality flow control	\$300	1	\$300	0	Parker fittings	Uah Mach shop
3/8 NPT X 3/8 NPT 90° adapter	\$5	1	\$5	\$5	ACE Hardware	ACE Hardware
Nipple 3/8 NPT	\$2	3	\$6	\$6	ACE Hardware	ACE Hardware
Hydraulic fluid (gal)	\$9	1	\$9	\$9	O'riellys	O'riellys
Hex bushing 3/8 by 1/2 NPT	\$4	2	\$8	\$8	ACE Hardware	ACE Hardware
			Subtotal	\$328	\$28	

Updated Cost Analysis Continued

Labor Costs					
	Labor description	Labor rate	Man hours	Retail Cost	Actual Cost
Engineering and design	Engineering research	\$80	15	\$1,200	\$0
	Engineering documentation	\$80	37	\$2,960	\$0
	Preliminary design	\$80	8	\$640	\$0
	CAD	\$80	16	\$1,280	\$0
	FEA analysis	\$80	20	\$1,600	\$0
				Subtotal	\$7,680
Manufacturing	Machining (adapter plates)	\$40	7	\$280	\$0
	Drilling (turning bars)	\$40	1	\$40	\$0
	Cutting and shaping of pieces	\$30	3.5	\$105	\$0
	Welding (interior spacers)	\$30	2.5	\$75	\$0
				Subtotal	\$220
Testing	Testing equipment turn radius	\$30	3	\$90	\$0
	Lift test of finished beam	\$30	3	\$90	\$0
				Subtotal	\$180
Assembly	Assembly of small slide	\$30	24	\$720	\$0
	Assembly of large slide	\$30	24	\$720	\$0
	Modifications of fork lift hydraulics	\$30	2	\$60	\$0
				Subtotal	\$1,500
Total Cost					
		Retail Cost	Actual Cost		
Totals	Channel beam (Design 4)	\$10,120	\$71		
	Grand total (Hardware and beam)	\$760	\$71		
	This reflects the cost to manufacture the beam with only materials and labor costs				

Updated Manufacturing Processes

- Duration

4 weeks (17 actual billable hours)

- Requirements

Cutting, Semi-Complex Machining, Drilling, Fitting, Welding

- Assistance Required

Hubbard & Drake, Team 1, Steve Collins

- Retail Cost - \$1,500

- Team Cost - \$0

Update Manufacturing Processes

- Manufacturing Location

Hubbard & Drake General Mechanical Contractors

P.O. Box 1867

1002 5th Ave SE

Decatur, Alabama 35602-1867

256.353.9244

www.hubbarddrake.com

- Initiation

Wednesday - September 22, 2010

Problems and Solutions

Problem 1: Original design included chains to wrap around the slide adapters. Special thanks to Scotty Hubbard and Jim Wahoski for pointing out that the chains could become entangled and create a safety hazard.

Solution 1: The chains have been changed to extension plates which will make the entire operation safer and easier.

Problem 2: Original fittings did not work on the Red lift.

Solution 2: New fittings were obtained and used to add the flow control valve.

Lessons Learned

- The most important lesson the team learned was to listen to experienced people when they give advice.
- Scottie Hubbard's advice to use the plates was given near the end of the previous 490 teams project.
- His advice was backed up this semester by Jim Wahoski, who also warned the team about using chains.
- This prompted the team to partially redesign their hardware. This became a big challenge to overcome and still stay on schedule.

Summary

- Going from chains to the extension plates was a positive
- Fabrication of the assembly by Hubbard & Drake was quick and professional.
- Installation of the small slide had a few small hiccups that were resolved with time.
- Installation of the large slide went hiccup free after learning from our mistakes on the small slide
- Team 1 is well pleased with the project outcome.

Acknowledgements

- Thanks to our customer, Mr. Tim Blackwell and the Center for Applied Optics
- Thanks to the shop foreman at Pro Fab fabrication in Hartselle, AL for the suggestion of using two pieces of C channel instead of an I beam.
- We would also like to thank Scottie Hubbard, of Hubbard and Drake General Mechanical Contractors in Decatur, AL, for offering raw materials and use of their shop equipment for this project.