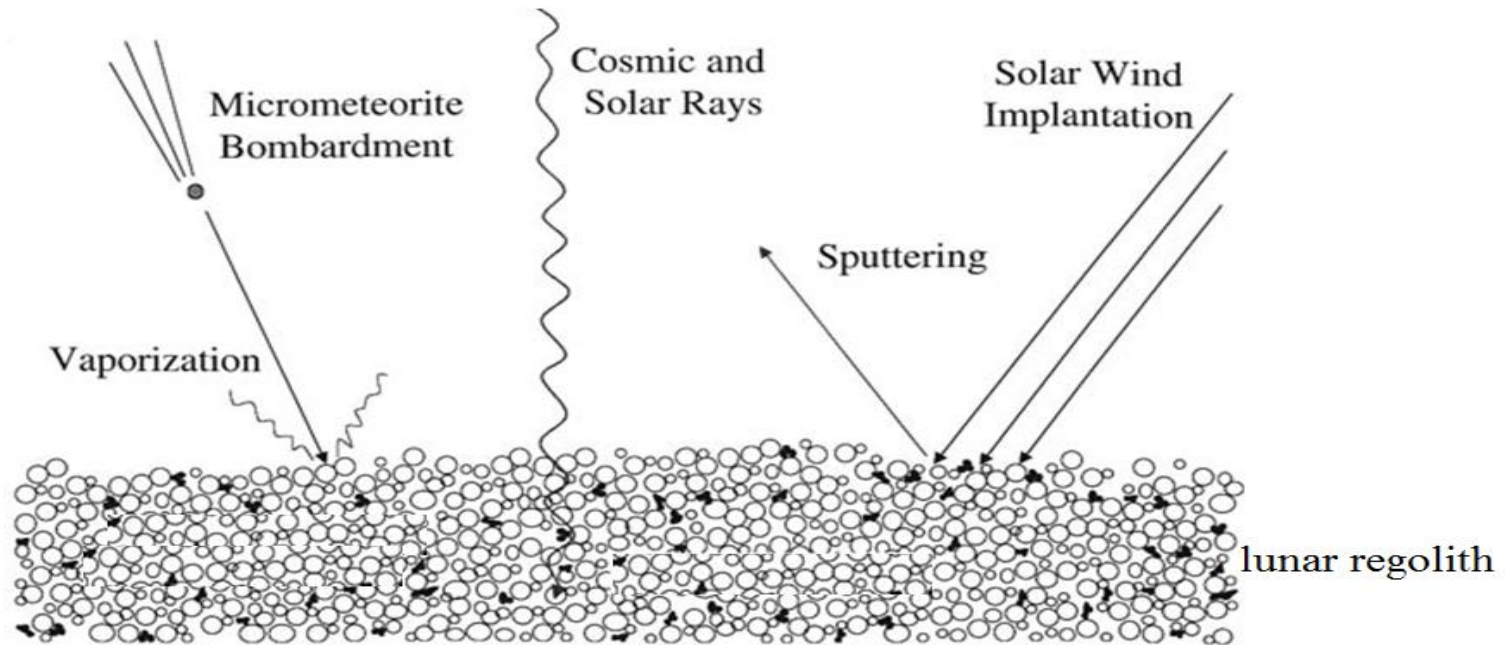


# **Sputtering of Lunar Regolith by Solar Wind Protons and Heavy Ions**

Samer Alnussirat

# Introduction

- Lunar surface material is accessible to the space weathering factors
- Solar wind protons and heavy ions with kinetic energies of about 1 keV/amu



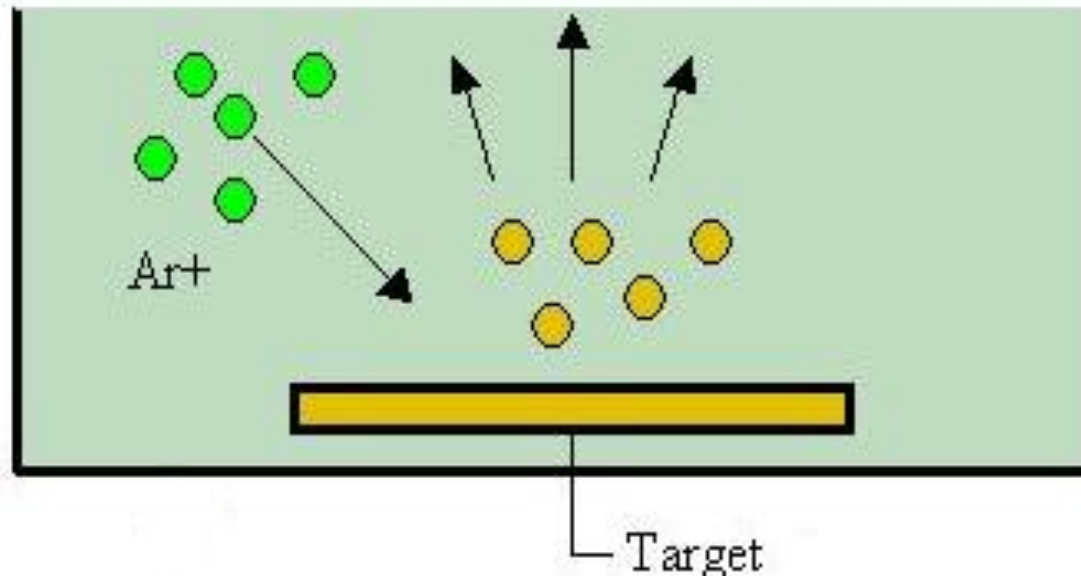
# Introduction

- At energies around 1 keV/amu, SW protons and HI interact with the lunar surface materials via a number of microscopic interactions, but for our purposes, the most important of these is atomic sputtering

# Physics of Sputtering

When the cascade gives the target atom energy greater than the surface binding energy, then the atom may be sputtered

$$Y_{ij} = \frac{\text{Number of sputtered atoms of material } i \text{ in the target}}{\text{Number of incident ions of type } i}$$



# Sputtering

```
graph TD; A[Sputtering] --> B["Kinetic Sputtering  
(Fast ions)"]; A --> C["Potential Sputtering  
(Slow multi charged ions)"];
```

**Kinetic Sputtering**  
(Fast ions)

**Potential Sputtering**  
(Slow multi charged ions)

# Lunar Regolith Simulant JSC-1A AGGL

XPS: Surface of the simulant consists mostly of oxides



Element	C	O	Si	Al	Fe	Ca	Mg	Ti	Na	P	K	Cr	F
Atomic %	2.3	55.6	19.5	8.4	1.4	4.3	3.9	0.4	3.3	0.3	0.3	0.1	0.1

# Heat-Conduction/Diffusion Equation

$$\frac{1}{\kappa} \frac{\partial u}{\partial t} = \nabla^2 u$$

Discretizing the space and time components in one dimension gives:

$$\frac{u(x, t+h) - u(x, t)}{\Delta t} = \frac{\kappa}{h^2} (u(x-h, t) - 2u(x, t) + u(x+h, t))$$

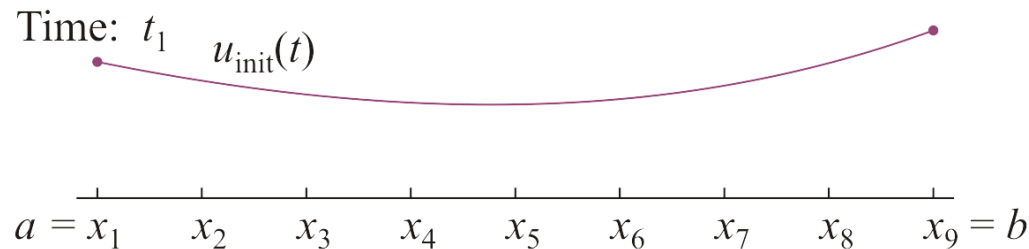
which allowed us to find

$$u(x, t+h) = u(x, t) + \frac{\kappa \Delta t}{h^2} (u(x-h, t) - 2u(x, t) + u(x+h, t))$$

# Method of Lines

As an alternative approach, associate with each spatial point an unknown function  $u_k(t)$

- Two exceptions:  $u_1(t) = a(t)$   
 $u_n(t) = b(t)$



This approach was popularized by the chemical engineer William E. Schiesser in his 1991 text *The Numerical Method of Lines*



# Method of Lines

In order to substitute  $u_k(t)$  into our mixed partial-/finite-difference equation,

$$\frac{\partial}{\partial t} u(x, t) = \frac{\kappa}{h^2} (u(x-h, t) - 2u(x, t) + u(x+h, t))$$

we note that the solution at location  $x - h$  is  $u_{k-1}(t)$  and the solution at  $x + h$  is  $u_{k+1}(t)$ :

$$\frac{d}{dt} u_k(t) = \frac{\kappa}{h^2} (u_{k-1}(t) - 2u_k(t) + u_{k+1}(t))$$

We also have the initial condition:

$$u_k(t_{\text{initial}}) = u_{\text{init}}(x_k)$$

# Systems of IVPs

We can therefore write this as:

$$\mathbf{u}^{(1)}(t) = \mathbf{f}(t, \mathbf{u}(t)) = \frac{\kappa}{h^2} \begin{pmatrix} \begin{pmatrix} -2 & 1 & & & \\ 1 & -2 & .1 & & \\ & 1 & -2 & \ddots & \\ & & \ddots & \ddots & 1 \\ & & & 1 & -2 \end{pmatrix} \mathbf{u}(t) + \begin{pmatrix} a(t) \\ 0 \\ \vdots \\ 0 \\ b(t) \end{pmatrix} \end{pmatrix}$$

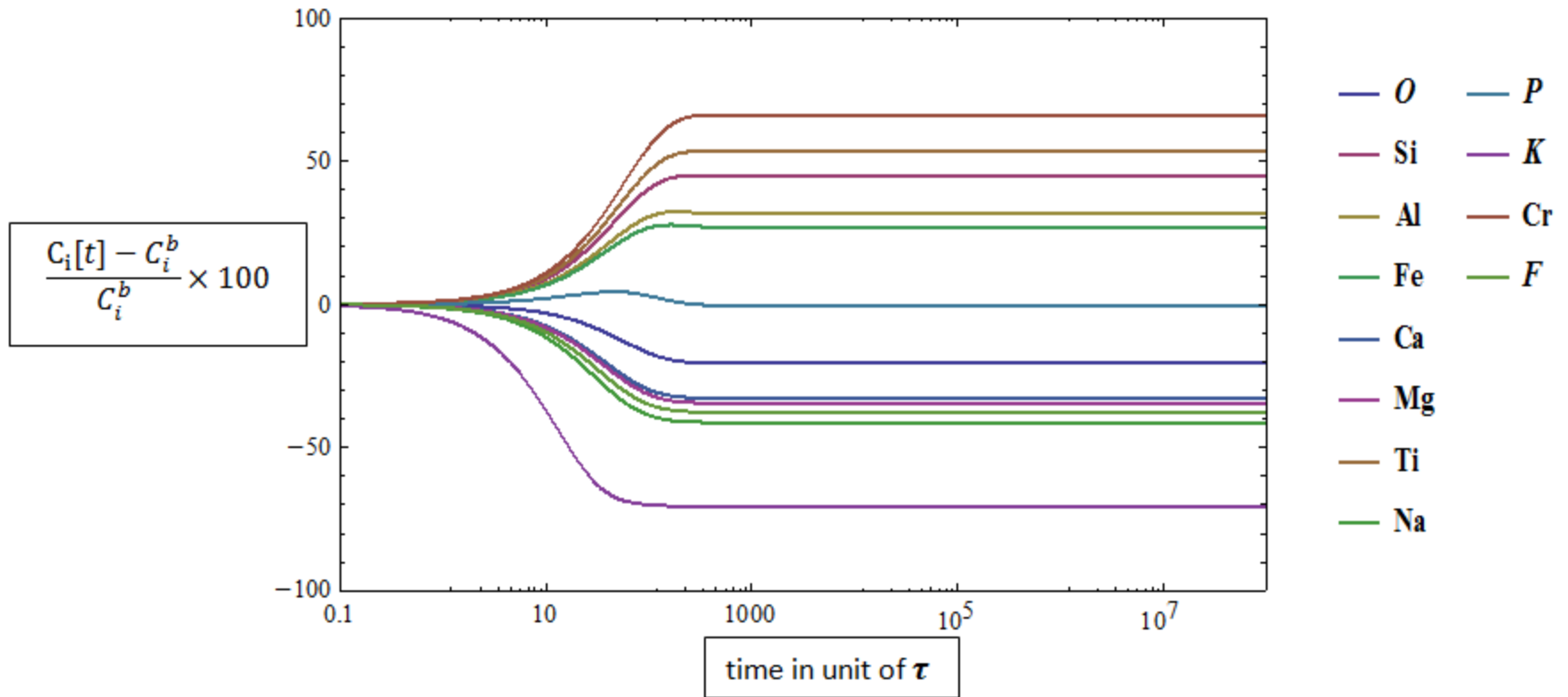
$$\text{where } \mathbf{f}(t, \mathbf{u}) \stackrel{\text{def}}{=} \frac{\kappa}{h^2} \begin{pmatrix} \begin{pmatrix} -2 & 1 & & & \\ 1 & -2 & .1 & & \\ & 1 & -2 & \ddots & \\ & & \ddots & \ddots & 1 \\ & & & 1 & -2 \end{pmatrix} \mathbf{u} + \begin{pmatrix} a(t) \\ 0 \\ 0 \\ 0 \\ b(t) \end{pmatrix} \end{pmatrix}$$

# Non-Equilibrium Model

$$\frac{dC_i}{dt} = \frac{1}{\tau} \left[ -C_i \sum_j Y_{ij} f_j + C_i^b \sum_k C_k Y_{kj} f_j \right]$$

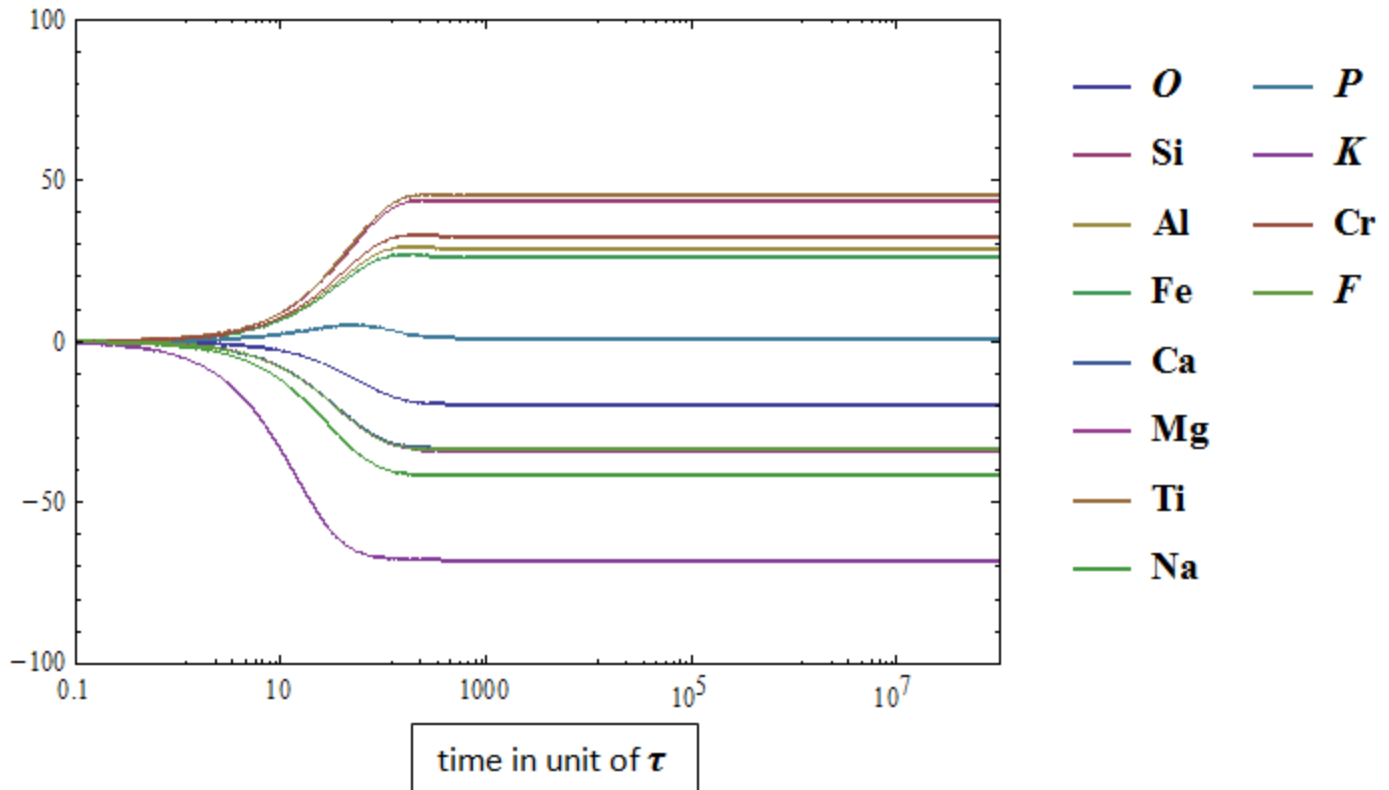
- $C_i$  is the abundant of element  $i$  in JSC-1A AGGL
- $C_i^b$  is the fractional abundant of element  $i$  in the JSC-1A AGGL bulk
- $Y_{ij}$  is the yield of element  $i$  by solar wind ion  $j$ ,
- $F_j$  is the fraction of solar wind  $j$  in the solar wind flux
- $\tau$  is a constant has dimension of time.

Calculated changes in the elemental composition of a JSC-1A AGGL surface as a function of time due to the kinetic sputtering of the solar-wind protons.



Element	O	Si	Al	Fe	Ca	Mg	Ti	Na	P	K	Cr	F
% Change	-20	+45	+29	+27	-32	-34	+53	-41	0	-70	+65	-39

Calculated changes in the elemental composition of a JSC-1A AGGL surface as a function of time due to the kinetic sputtering of the solar-wind protons and heavy ions.



$$\frac{C_i[t] - C_i^b}{C_i^b} \times 100$$

Element	O	Si	Al	Fe	Ca	Mg	Ti	Na	P	K	Cr	F
% Change	-19	+47	+29	+27	-32	-32	+45	-41	0	-69	+32	-33

# Conclusions

- Sputtering is an important dynamic mechanism that affects the composition of both the lunar surface and its tenuous exosphere.
- The contribution of the solar-wind protons and ions kinetic sputtering to the changes in the composition of the surface layer of the oxides of the lunar surface is well understood and modeled
- we expect these changes to be more than the calculated due to contribution of the potential sputtering which is unclear.

# Conclusions

- The changes in the elemental abundance of JSC-1A AGGL due to the solar wind protons alone approach the steady state for times close to  $300T$ , and this time shortened to about  $200T$  due to the heavy ions contributions